

A short tutorial by R. Scholten

#### Measuring something

- Common task: measure light intensity, e.g. absorption spectrum
- Need very low intensity to reduce broadening
- Noise becomes a problem



Rb spectrum

# The principle

- Fundamental law of communication theory: *Wiener-Khinchin* theorem
- Reduction of noise imposed upon a useful signal with frequency f<sub>0</sub>, is proportional to the square root of the bandwidth of a bandpass filter, centre frequency f<sub>0</sub>





### Measuring something

- Need to measure at high frequency, where noise is low
- Modulate signal, look for component oscillating at modulation frequency



#### Signal from noise

- A *lock-in amplifier* is used to extract signal from noise
- It detects signal based on modulation at some known frequency
- Premise:
  - much noise at low frequency (e.g. dc), less noise at high frequency
  - measure within narrow spectral range, reduce noise bandwidth
- Hence shift measurement to high frequency



## Demodulator or PSD (phase-sensitive detector)



#### Mathematical description

Signal  $V_{\rm s}(t)$  varies relatively slowly e.g. absorption spectrum scan over 10 seconds





 $V_{\rm ref} = \cos(\omega t + \phi)$ 

- Modulate at relatively high frequency  $\omega$  (e.g. chopper):  $V_{sig} = V_s(t) \cos \omega t$
- Reference (local oscillator) of fixed amplitude:
  - phase  $\phi$  is variable
  - oscillator frequency  $\omega$  same as modulation frequency
- Multiply modulated signal by REF :  $V_{sig}V_{ref} = V_S(t)\cos\omega t\cos(\omega t + \phi)$ =  $\frac{1}{2}V_S(t)\cos\phi + \frac{1}{2}V_S(t)\cos(2\omega t + \phi)$
- Second term at high frequency  $(2\omega)$
- Low-pass filter (cutoff ~  $\omega/2$  or lower)



### Some details

Simple trig

$$\begin{split} V_{\text{ref}} V_{\text{sig}} &= V_S(t) \cos \omega t \cos(\omega t + \phi) + n(t) \cos(\omega t + \phi) \\ &= V_S(t) \cos \omega t [\cos \omega t \cos \phi - \sin \omega t \sin \phi] + \dots \\ &= V_S(t) [\cos^2 \omega t \cos \phi - \cos \omega t \sin \omega t \sin \phi] + \dots \\ &= V_S(t) [(\frac{1}{2} + \frac{1}{2} \cos 2\omega t) \cos \phi - \frac{1}{2} \sin 2\omega t \sin \phi] + \dots \\ &= \frac{1}{2} V_S(t) [\cos \phi + \cos 2\omega t \cos \phi - \sin 2\omega t \sin \phi] + \dots \\ &= \frac{1}{2} V_S(t) \cos \phi + \frac{1}{2} V_S(t) [\cos 2\omega t \cos \phi - \sin 2\omega t \sin \phi] + \dots \\ &= \frac{1}{2} V_S(t) \cos \phi + \frac{1}{2} V_S(t) [\cos (2\omega t + \phi) + n(t) \cos(\omega t + \phi)] \end{split}$$

#### Noise

- Noise reduces with frequency (1/f noise is major problem)
- Shift signal to higher frequency
- Noise within given bandwidth reduces as we measure at higher frequency







www.technion.ac.il/technion/chemistry/courses/w05/127421

# With noise

- Signal has noise:  $V_{sig} = V_s(t) \cos \omega t + n(t)$
- Multiply reference by modulated signal:

$$V_{\text{ref}}V_{\text{sig}} = V_{s}(t)\cos\omega t\cos(\omega t + \phi) + n(t)\cos(\omega t + \phi)$$
$$= \frac{1}{2}V_{s}(t)\cos\phi + \frac{1}{2}V_{s}(t)\cos(2\omega t + \phi) + n(t)\cos(\omega t + \phi)$$

- Third term noise at frequency  $\omega$
- Low-pass filter, frequency less than  $\omega/2$ , leaves signal components
- We win twice:
  - less noise at  $\omega$
  - reduce bandwidth

#### Using PSD oscillator to modulate



#### External modulator: true "lock-in"



#### Further details

- True lock-in amp can work with external oscillator for Reference:
  - Input reference from external experiment
  - Use phase-locked-loop to generate stable local oscillator
- Lock-in amp has variable post-multiplier (low-pass) filter
  - Time constants: what time constant is appropriate?
  - Shapes (6<sup>th</sup>, 12<sup>th</sup>, ... order): which is best?
- If input signal has *harmonics* (e.g. due to imperfect modulation) then will detect spurious signal
  - Use *input* filter to minimise
- Dynamic reserve?

#### Other applications

- Often use lockin to measure response function of actuator (or similar)
- Two-channel lockin measure signal and phase
- Phase  $\rightarrow$  resonances



#### **Experiments**

- Photodiode + LED
- SRS FFT spectrum analyser
- Oscilloscope
- Switch LED on/off, e.g. with hand to block
- HP function generator to modulate LED
- And/or chopper
- SRS lock-in amp



Frequency modulation

#### Derivatives: Lock-in amps & feedback servos

- So far, we have modulated *amplitude*, and used LIA to demodulate
- PSD (lockin) = fancy bandpass filter?!
- Can also use *frequency* modulation (like FM radio)
- Let's measure  $V_{\rm s}(\omega)$  i.e. a spectrum, where we slowly vary  $\omega(t)$
- Frequency-modulate:  $\omega(t) = \omega_0 + \Omega_0 \cos \Omega t$ where  $\Omega$  is the modulation (Fourier) frequency
- Using Taylor-series expansion:  $V_s(\omega) = V_s(\omega_0) \left(\frac{dV_s}{d\omega}\right) \left(\Omega_0 \cos \Omega t\right) + \dots$
- Note two things immediately:
  - dc component is same as un-modulated spectrum
  - ac component is *proportional to derivative* of spectrum

#### Extract derivative with PSD/lock-in amp

• We now multiply our signal by our reference, as before:

• Note *modulation* at  $\Omega$ , and fixed  $\omega_0$  i.e. slowly varying laser frequency

$$V_{sig}V_{ref} = V_S \cos(\Omega t + \phi) + \frac{dV_S}{d\omega}\Omega_0 \cos\Omega t \cos(\Omega t + \phi)$$
  
=...  
$$= V_S \cos(\Omega t + \phi) + \frac{1}{2}\Omega_0 \frac{dV_S}{d\omega} \cos(2\Omega t + \phi) + \frac{1}{2}\Omega_0 \frac{dV_S}{d\omega} \cos\phi$$

• Again: low-pass filter (cutoff ~  $\omega/2$  or lower)

$$V_{\rm sig}V_{\rm ref} \approx \frac{1}{2}\Omega_0 \frac{dV_s}{d\omega}\cos\phi$$

- We have a measurement proportional to the *derivative*
- Measurement *changes sign* if slope changes sign: dispersion
- Note: modulation depth  $arOmega_0$  must not be larger than peak in spectrum!
- Higher-order terms in Taylor expansion: can measure 2<sup>nd</sup> deriv, 3<sup>rd</sup> deriv, etc.

#### Lock-in amplifiers and feedback servos

• Example: Lorentzian peak in atomic absorption spectrum





Modulated output from detector





Spread-spectrum

#### PRBS: Lock-in on steroids!

- Lock-in uses small part of spectrum
- Can use broad spectrum and still separate signal from noise
- Pseudo-random bit sequence
  - Spread-spectrum communications
    - computer 802.11 wireless, etc.
    - CDMA telephones
    - Modems
  - Security/encryption
  - Acoustics



#### SPREAD-SPECTRUM MODULATION

- all frequencies present simultaneously in modulation function
- phases adjusted so that components add in quadrature

http://www.chm.bris.ac.uk/pt/mcinet/sum\_schl\_02\_docs/tof.ppt



20 frequencies random phases

 truly random phases cause excursions out of range ⇒ use *pseudo-random* functions

#### Spread-spectrum history



Also famous as first nude in cinemarelease movie!

- Hedy Lamarr (1913-2000), composer George Antheil (1900-1959) patented submarine communication device
- Synchronized frequency hopping to evade jamming
- Original mechanical action based upon pianolas
- Used today in GPS, cellphones, digital radio



#### Binary pseudo-random sequences





http://www.chm.bris.ac.uk/pt/mcinet/sum\_schl\_02\_docs/tof.ppt

#### PRBS: Lock-in on steroids!

- Generate signal in pseudo-random bit sequence, for example:
  - 6-bit (64-bits long)
  - 8-bit (256 bits long):
- Record signal
- Multiply by PRBS (auto-correlate)
- Very much like a lock-in! But uses broad spectrum



#### 13-bit (8192 bits long) MLS single scan

